

TASK CLOSE OUT DOCUMENT

Task Scope NATURAL CIRCULATION - DEGRADED  
CORE GEOMETRY - CALCULATION OF  
TEMPERATURES

To: M. Levenson  
S. Levy  
E. Zebroski

Task No. 29

Date Complete 4/21

Reason felt task is complete:

preliminary temperatures calculated  
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Members of Committee

Reviewed at EPRI under  
W. Levenson  
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W. Levenson for S. Levy  
Signed  
Committee Leader

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To: M. Lovan son

From: Wilhoisenstein

NATURAL CIRCULATION/DEGRADED CORE EXPERIMENT

OBJECTIVE: To ascertain the efficiency of cooling by free convection within degraded core.

ASSUMPTION: (1) Fuel has collected in layers over central core region at grid spacer elevations. (15 inches apart)

(2) Heat generation rate of  $1.5 \times 10^{-3}$  of nominal full power (2732 MW).

(3) Total blockage of central core region (annular bypass of scaled dimensions)

a) 3/4 blockage

b) 7/8 blockage

SOLUTION: (1) Use Volume Scaling (i.e. KW/ft<sup>3</sup> water)

(2)  $Q_{\text{core}} = 4.1 \text{ MW}$

$Q_{\text{layer}} = 450 \text{ KW (9 layers)}$

$\frac{Q_{\text{Layer}}}{V_{\text{Layer}}} = 6.3 \frac{\text{KW}}{\text{ft}^3}$

} Target TMI

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Test Vessel I.D. = 9 inches

Test Pressure = Atmospheric

Plate to Wall Gap = 0.300 in. (3/4 Blocked)

Plate to Wall Gap = 0.150 in. (7/8 blocked)

Target Test Model Q = 0.23 KW/layer

Spacing between layers = 1.25 inches

} Test Model

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$Q_{\text{layer}} = 0.21 \text{ KW/layer}$

$Q_{\text{layer}} = 0.40 \text{ KW/layer}$

$Q_{\text{layer}} = 0.67 \text{ KW/layer}$

} Achieved

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RESULTS: (1) Boiling not observed anywhere during free convection.

(2) Threshold of local boiling (top layer) only observed when inlet flow reduced by use of valve.

(3) See Figure attached for actual results.

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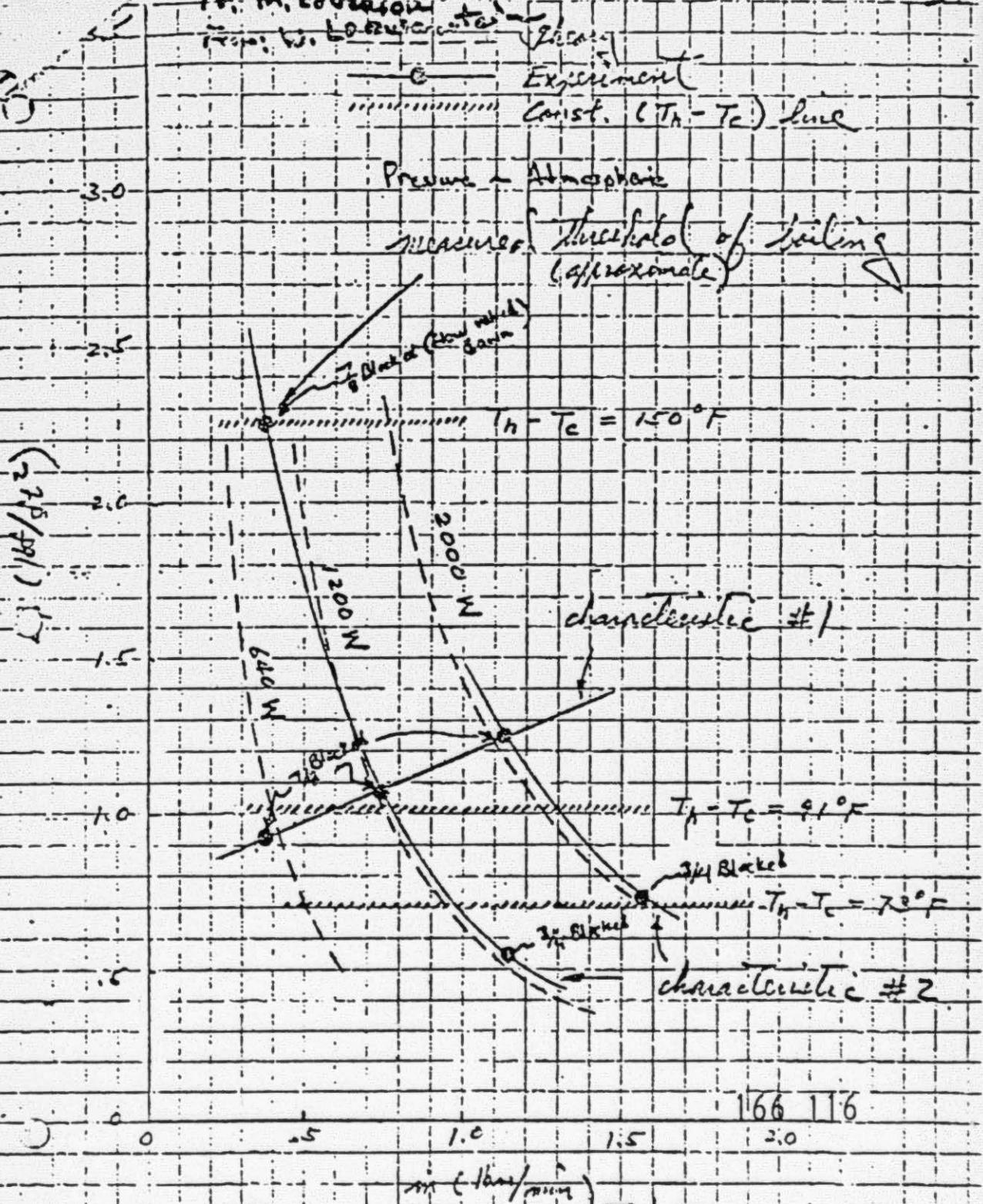


Fig. 2 System Characteristics

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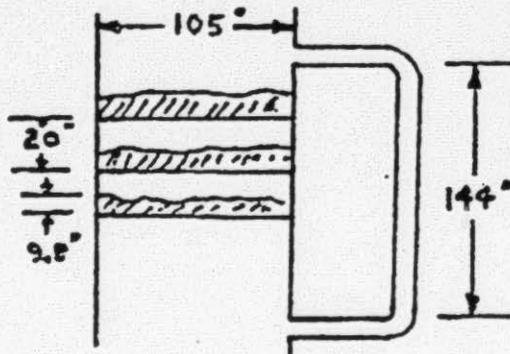
Free Convection Heat Transfer Calculations  
Through "Porous" Media

A. Calculate four cases:

1. System pressure = 900 psi  
Inlet temperature =  $280^{\circ}\text{F}$  and  $350^{\circ}\text{F}$
2. System pressure is atmospheric  
Inlet temperature =  $170^{\circ}\text{F}$  and  $200^{\circ}\text{F}$

Assumptions:

1. Power  $\approx 0.2\%$  of 2500MW  $\approx 6\text{MW}$
2. Core divided into 8 regions defined by spacers.
3. Region with porous medium has diameter of 105 in.
4. Porous medium is defined by cylinders of .4" diameter spaced with a pitch to diameter ratio of 1.065 in a staggered grid. This gives a porosity of 20%. For heat transfer area the ends of the cylinders are ignored.
5. Assume 3 "trays" of porous material, in following geometry.



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Results:

1. The heat transfer rate required in the porous medium is 306 BTU/hr ft<sup>2</sup> to carry away the heat generated. (If a temperature difference of  $100^{\circ}\text{F}$  is

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Results (cont.):

assumed between the fluid and the surface, the heat transfer coefficient required is about  $3 \text{ BTU/hr ft}^2$  which is typical of free convection in air.)

2. At a pressure of 900 psi, free convection provides more than enough flow at inlet temperatures of  $280^\circ\text{F}$  and  $350^\circ\text{F}$  to prevent the water from reaching saturation. The heat transfer coefficient is of order  $250 \text{ BTU/hr ft}^2$  and the temperature rise approximately  $1^\circ\text{F}$ .
3. At atmospheric pressure with inlet temperature of  $170^\circ\text{F}$  or higher, free convection does not provide enough flow to allow water to remain sub-cooled. Hence local boiling will result.
4. Calculations using CHF correlations for beds consisting of 300 to 800 micron particles show that at atmospheric conditions CHF will probably be reached. However, due to the low power generation the temperature rise will not be significant.