

*Voice**File*

TASK CLOSE OUT DOCUMENT

Task Scope Review of Sandia IWR/C
Emergency Containment Vent
Design Package

To: M. Levenson
S. Levy
E. Zebroski

Task No. _____

Date Complete 7-16-79

Reason felt task is complete:

Review complete, to the extent consistent
with lack of design detail. Comments
attached.

Members of Committee

James W. Thringa
JJames W. Thringa
Signed
Committee Leader

162 298

To: Milt Levenson
Subject: Emergency Containment
Venting Package

Date: April 16, 1979
From: J. W. Thiesing

Comments on emergency containment venting package received from Sandia/NRC follow:

- (1) Page 1 - 10^6 Ci I release represents about 10% of current total activity of I-131 (core & RCS) seems reasonable - given core melt (no containment or vessel cooling) and containment failure above grade.
- (2) Page 2 - "Steam-condense" and "steam-no condense" labels appear to be interchanged.
- (3) Page 3 - Containment pressure -
Spike up to 70 psig at 374 hours is too fast. Would expect only about a 12 psig per hour 'superheat from core heat) at today's decay heat level. I do not understand rapid drop in containment pressure after vessel failure (no cooling of containment was assumed). Pressure would remain constant at 70 psig until debris heated water pool in containment and began steaming. End result is the same, however, failure above grade.
- (4) Page 4 - Appears to postulate 20% Core I-131 becomes airborne.
- (5) Page 5 - System Design
 1. All air handling systems should be designed for 150 psig if maximum utility is to be gained (150 is probable containment failure pressure).
 2. What is purpose of N₂ system - I presume it is inerting for H₂, but the utility of this is questionable. (Prevent H₂ burn in exhaust line, I suppose).
 3. 3×10^6 Btu/hr cooling on diffuser tanks will not keep up with decay heat until about July 1, 1979.
 4. Why install return line to containment. The presumption of containment overpressure mitigates against its use except as a routine cleanup tool! If there is urgency to install this system, it can probably not be well-enough thought out to serve as the ultimate clean up mechanism.
 5. Diffuser tanks should be buried in yard outside aux building. Line from containment to diffuser tanks should also be buried. Cooling system must also be shielded.
 6. Need valves in filter bypass.

(6) Page 6 - Options

1. Backup filters (Option 2) will require demisters, and could defeat system by becoming clogged - Recommend HEPA only, with bypass capability.
2. Option #3 - There is not a recombiner in the world that will handle the flow rates that will be required.

Milt Levenson
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3. Option #4 - Should not put tanks in fuel pool - it's being used for tank farm. Also, violates last constraint on page 7.
4. Option #6 - What is a "Hydrogen combustion mechanism."

4/15/77

J. Thising

There are variations in
contaminant usage in the different
2 min. zones.

Please understand and give
comments to M. Levinson in present
to R. Arnold.

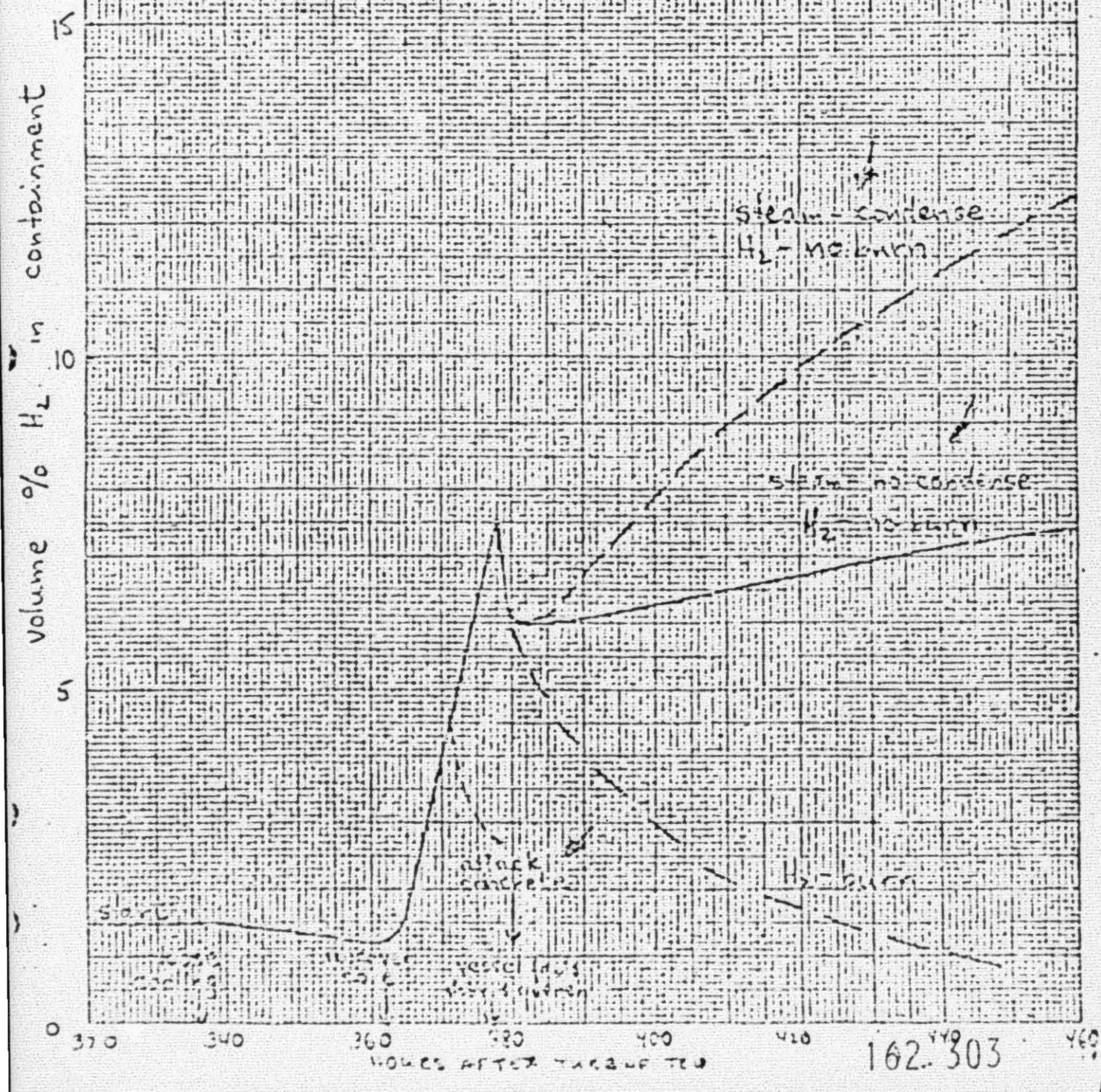
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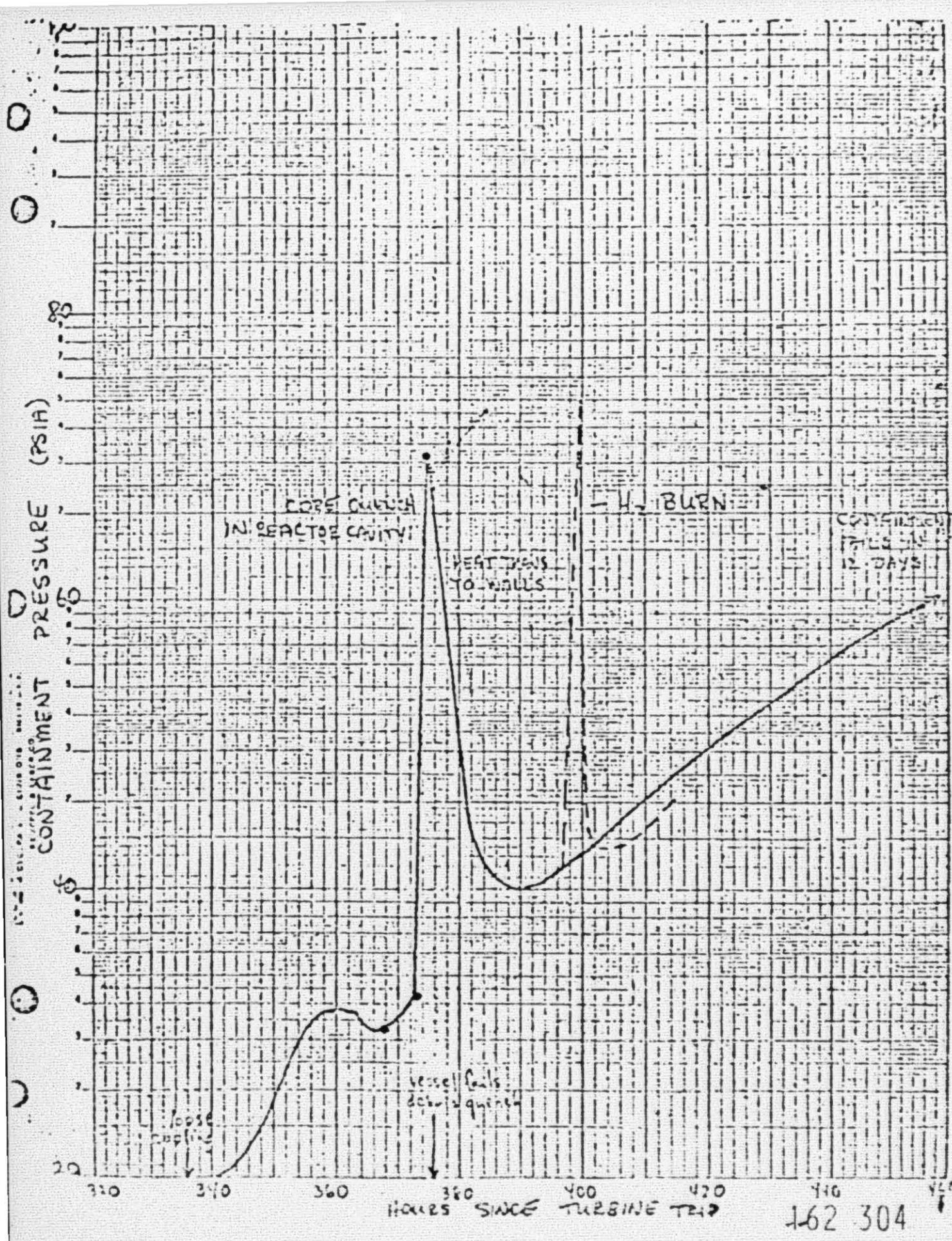
RADIOLOGICAL CONSIDERATIONS

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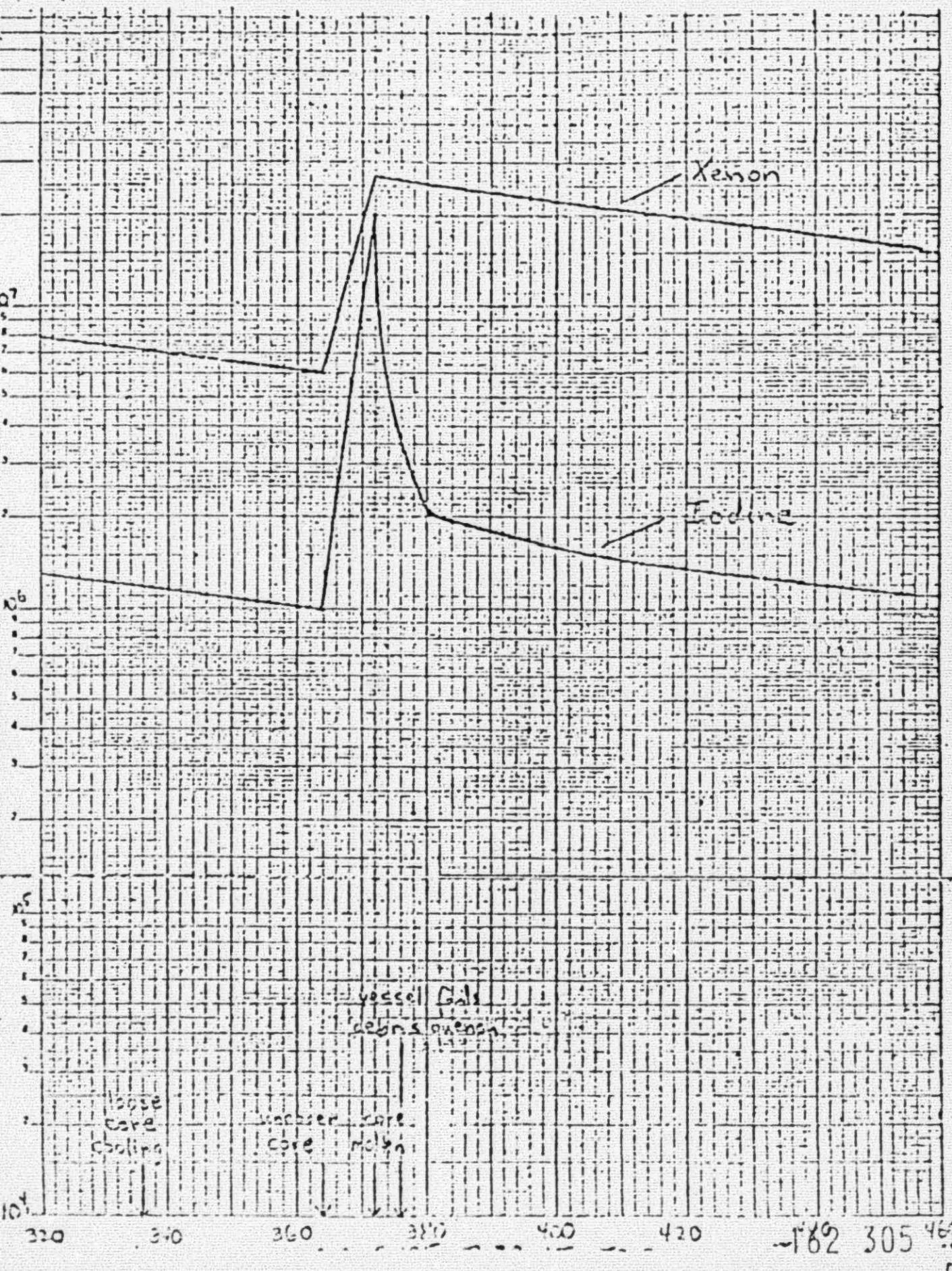
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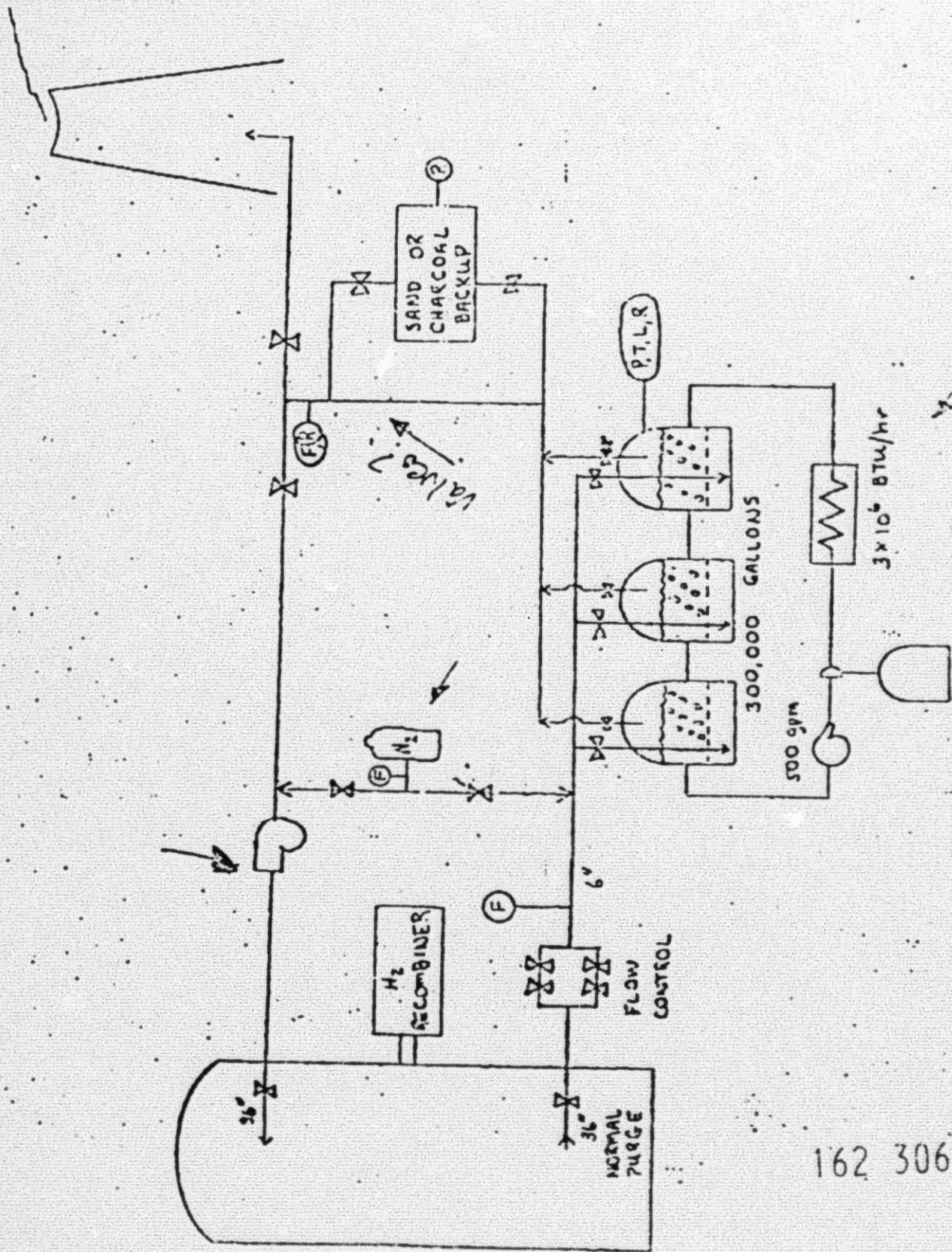


QUERIES AIRBORNE IN CONTINUOUS

10⁻²
10⁻³
10⁻⁴
10⁻⁵
10⁻⁶
10⁻⁷
10⁻⁸
10⁻⁹
10⁻¹⁰



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CONSTRUCTION OPTIONS

OPTION 1 : AS SHOWN

OPTION 2 : DELETE BACKUP FILTERS

OPTION 3 : INSTALL ADDITIONAL H₂ RECOMBINERS DOWNSTREAM OF SCENARIOS

OPTION 4 : PUT SPENT FUEL POOL IN SPENT FUEL POOL #2

OPTION 5 : DELETE RECIRCULATION LINE TO CONTAINMENT

OPTION 6 : ADD HYDROGEN COMBUSTION MECHANISM

9256

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TASK: CONCEPTUAL DESIGN OPTIONS FOR TMI-2 CONTAINMENT VENTING

ASSUMPTIONS: CORE MELT INITIATED AT T = 14 DAYS
NO CONTAINMENT COOLING OR SPRAYS

FUNCTIONAL REQUIREMENTS: MAINTAIN CONTAINMENT INTEGRITY
MINIMIZE RELEASE OF RADIONACTIVITY

CONSTRAINTS: TIME TO CONSTRUCT (DAYS)
OCCUPATIONAL EXPOSURE
MINIMIZE AUXILIARY BUILDING CONTAMINATION

ALL BACK ON 4/1-8377
WITH COMMENTS BY 4/14 3PM
~~4/14-8377~~

TO: TOM TELFORD
TEL - 8976

FROM: R. DISALVO
DATE: 4/14/79 12:30 P.M.
TIME: