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Ane 7, 1989 4410-89-L-0064/0190P

US Mauleur Regulatory Commission Attn: Dougest Control Desk Washington, OC 20555

Dear Sirs:

Three wile Island Haller Station, Duit 2 (INI-2)
Operating Liumse Mo. UTH-73
Ocuset No. 50-320
Arrawl Update of Residor Suilding Surp Revirculation
System Description

As requested by MRE Letter dated February 4, 1987, GPU Martear has performed the annual review of the Reacter Building Sump Reliquistion System Description. Revision 1 of the system description is attached for your information.

Sincerely.

M. B. Rosen Director, IMI-2

EDS/enf

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DIVISION SYSTEM DESCRIPTION FOR

Reactor Building

| Sump | Recirculation System | (RRS) | |
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System Description for Reactor Building Sump Recirculation System

Page 2 of 14

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TABLE OF CONTENTS

| SECT | ION | | Page | |
|---------|--------------------|---|------|-----|
| 1.0 | SYSTEM DESCRIPTION | | | |
| | 1.1 | Summery | 3 | |
| | 1.2 | References | 3 | |
| | 1.3 | Detailed System Description | 4 | |
| | 1.4 | System Performance Characteristics | 6 | |
| | 1.5 | System Arrangement | 6 | |
| | 1.6 | Instrumentation and Controls | 7 | |
| | 1.7 | System Interfaces | 7 | |
| 2.0 | SYSTI | M LIMITATIONS, SETPOINTS, AND PRECAUTIONS | 8 | |
| 1.0 | OPER | OPERATIONS | | |
| | 3.1 | Operation in the Euroine Building (Technical | 8 | |
| | | Specifications Surveillance) | | |
| | 1.2 | Operation in the Reactor Building | 9 | |
| 4.0 CAS | CASU | UALTY EVENTS AND RECOVERY PROCEDURES | | |
| | 4.1 | Casualty Events | to | |
| | 4.2 | Design Features to Mitigate Effects of Casualty Events | 11 | |
| | 4.3 | Recovery Procedures | - 11 | |
| 5.0 | MAIN | MAINTENANCE | | |
| | 5.1 | Corrective Maintenance | 11 | |
| | 5.2 | Preventive Maintenance | 12 | |
| | 5.1 | Survettlance | 12 | |
| | 5.4 | In-Service Insception | 12 | |
| 6.0 | testing | | 12 | |
| 7.0 | HUH | n FACTORS | 12 | |
| Tabi | le 1 | Reactor Building Sump Recirculation Pumps (RRS.P.1A, RRS.P.1B, Spare) | 13 | 100 |
| fig | re l | Reactor Building Sump Recirculation Pumps (RRS-P-1A, RRS-P-1B, Sparm) | 18 | |
| | | | | |

1.0 SYSTEM DESCRIPTION

1.1 Summary

The Reactor Building Summ Recirculation System (RES) is a non-telimic contingency system ready for installation in the event of an unisolable leak from the Reactor Vestel. The system uses two 200 gpm submersible pumps, associated hoses and controls to transfer eater from the Reactor Building besement to the Reactor Vestel. The RRS is designed to maintain sufficient water in the Reactor Vestel to heep the core covered for leak rates up to 400 gpm. The system components are staged in a clean, dedicated area of SML-2. Electrical connections for each pump are preinstalled in the Reactor Building with breakers and remote traiters located in the relay room.

1.2 References

- 1.2.1 General Arrangement, Reactor Guilding Sump Recirculation System General Arrangement and Control Manifold Details, Drawing ZE-1510-1025.
- 1.2.2 CPU muclear Letter. 4410-84-L-0154, Technical Specification Change Request No. 46, November 6, 1984.
- 1.2.3 IM1-2 Technical Specifications.
- 1.2.4 Instruction Manual, MCDA Pump Notel # 1707.
- 1.2.5 P and ID. Reactor Building Sump Rectrculation System, Orawing 2E-3510-1024.

1.3 Detailed System Description

1.3.1 Design Requirements

The RRS is an emergency system dasigned to transfer water from the Reactor Building basement to the Reactor Metical. Its objective is to keep the core covered during an unicolable Reactor Messel leak. The system is staged in a radiologically clean as a of IMI-2 and is required by the Technical Specifications.

The system design is based on the following requirement: and assumptions per Reference 1.2.2:

- of the most probable Reactor Vessel Irek is a corrosion type failure of an incore tube. The corresponding less rate is 17 gpm. An additional tube fatis rach wonth increasing the vessel less rate to 200 gpm one year efter the first failure.
- o Access to the Reactor Building is permitted during the leab.
- o The Reactor Sullding sump must be borated to 4350 ppm minimum, refirculated, and sampled prior to injection into the Reactor Vessel.

- The Borated Mater Storage Tank ' WSI') can be used to makeup the leak until the sump is adequately borated and the BRS installed.
- o The RRS should be capable of delivering up to 400 gpm and have backup to cover postulated single active failures. Both the primary and backup system should be staged on site and be as simple as possible.

The RRS is intended as a temporary means of emergency makeup. If the vessel leak cannot be repaired on the fuel cannot be removed within 6 to 12 months after the initial leak, it is assumed that a permanent recursulation system will be designed and installed or an existing plant system reactivated.

1.3.2 System Operation

The RRS consists of an "A" and "8" train, each capable of delivering up to 200 gpm. Each train is combrised of a 200 gpm submersible pomp (RRS-P-18 and RRS-P-18), a flow indicator (RRS-FL-1a), a throttle valve (RRS-Y-1A and RRS-FL-1B), a throttle valve (RRS-Y-1A and RRS-Y-1B), a pressure indicator (RRS-Y-1A and RRS-Y-1B), a pressure indicator (RRS-P1-1A and RRS-Y-1B), a pressure indicator (RRS-P1-1A and RRS-Y-1B), a pressure indicator (RRS-P1-1A and RRS-Y-1B), and approximately 150 feet of 2 1/2" 10 rubber hose. The valves and instrumentation are mounted on a mobile frame referred to as the Control manifold. A spare pump and spare hose are also growides.

Submersible pumps RRS-P-IA and RRS-P-IB are used to either recirculate the Reactor Building sump mater or to transfer sump water to the Reactor Vessel. The pumps take suction directly off the Reactor Building basement floor and are capable of pumping all solids that can pass through their inlet strainers. The pumps are connected to the inlets on the control manifold by separate 2 1/2" ID discharge houss. The control manifold provides throttling. flow indication, and sampling capabilities for each pump.

If desirable, the summers and hose can be used without the control manifold; flow could be controlled by starting and stopping the bumps as required.

Moses are also connected to the two outlets on the control manifold. These hoses insitelly are routed back to the Reactor Building basement to provide for rectriculation of the sump water. Sump water is rectriculated at a rate of up to 400 gpm using two trains, when the sump is adequately Milead, the hotes are rerouted to the Reactor Vessel to provide for continuous makeup of a Reactor Vessel to provide for continuous makeup of a

Reactor Vestel leaks of less than 200 gpm require only the "A" train for makeup. The "B" train serves as becaup for single active failures. Leaks exceeding 200 gpm require both trains for makeup. The spare puep and spare hose provide becaup for single active failures.

The system pumps are operated from remote starters located in the relay room. Each starter is supplied from a Class IE power source.

1.3.3 System Components (See References 1.2.1 and 1.2.5)

1.3.3.1 Pumps (See Table 1 and Figure 1)

Two MEDA model no. 1707 submersible pumps (BRS-P-IA and BRS-P-IB) provide the pumping power to recirculate the Reactor Building sump water or to transfer summ water to the Reactor Vessel. The pumps ere single stage, top discharge, vertical shaft cantrifugal type, fach pump weight 210 powrids. The pump motors and starters are contained in the pump housing. Built-in thermal motor protection automatically break the motor current if the motor temperature exceeds 105°F. The pumps are free standing and are provided with 66 feet of electrical cord. The pump sixcharges have female case locking type duick couplings for connection to the system hotes. A third, identical comp is provided as a spare.

1.3.1.2 Nose

Three hundred feet of Goodall N-2427 (PDN Agricultural hose is used to transport the summ water. The hose has a rated working pressure of 150 psig, a minimum bend radius of 10 inches, and is 2 1/2° 10. The hose is provided in two 50 foot and two 100 foot lengths. The ends of each hose are fitted with male stainless steel can locking type quick couplings. Two additional 50 foot lengths and one 100 foot length are provided at spares.

1.3.3.3 Control Hantfold

1.4 System Performance Characteristics

System performance characteristics are as follows:

- design flow rate is 400 gon (200 gon ger train);
- b. normal system operating pressure et the design flow rate is 70 psig maximum (see Figure 1 for pump head Curves)
- c. delign pressure is 150 pstg
- d. design temperature is 100°f.

1.5 System Arrangement

1.5.1 Stagles Arrangement

When the BRS is not required, the hoses, pumps, and control manifold are staged in a radiologically clean, dedicated area of TML-2. An electrical outlet for eath psymp is permanently installed in the Reactor Building near the 3C5' elevation batch by the air coolers. Starters located in the relay room provide power to the electrical outlets.

1.5.2 Operating Arrangement (See References 1.2.1 and 1.2.5)

During a Reactor Yessel leak, the pumps are located on the 282° elevation of the Reactor Suliding, directly tellow the Ratch at elevation 305°. The control manifold is located near the hatch on the 305° elevation. Two 50 foot hoses are mouted between the pumps and the control manifold. Two 100 foot hoses are routed from the control manifold to either the seismic gap in the morthwest portion of the Reactor Suliding to rectriculate sump water or to the Internals Indexing Fiature tilf? to transfer sump water to the Reactor Vessel. A spare pump and spare hoses are steamd in the Turbine Building.

1.6 Instrumentation and Controls

1.6.1 Flow Indicators

Flow indicators, RRS-FI-1a and RRS-FI-18, are provided to monitor the flow rates of pumps RRS-P-1A and RRS-P-1B respectively. Their range is 0 to 200 gpm in increments of 20 gpm. Flow rates exceeding 200 gpm will not affect calibration nor damage the flow indicators.

1.6.2 Pressure Indicators

Pressure indicators, RRS-PI-IA and RRS-PI-IB, are provided for verification of pump head characteristics. Their range is 0 to 300 pxig.

1.6.3 Electrical Power

Electrical power for the sumps is provided through outlets initialled near the 305' elevation hatchway. Each outlet is energized from a separate starter located in the relay room. Power for each starter is obtained from a Class II Power Distribution Panel. Class II and non-Class II solution is provided at the Sanels by circuit Breakers.

1.7 Sestin Interfaces

The RRS interfaces with the following systems:

- a. Defueling fest Assemly (DIA) or other suitable tank for testing
- b. a temporary power supply in the Turbine Building
- c. Reactor Contant System (RCS)
- d. A Class IE electrical system
- 1.7.1 Interfaces with the DTA tank, or other suitable tank, and a temporary power supply occur only during performance of the Technical Specification Surveillances. These interfaces allow for convenient testing of the pumps and instrumentation.
- 1.7.2 Interfaces with the RCS and the Class IE electrical system is required if the RRS is placed in service. Plug type connectors are used to tie-in to previously installed, dedicated electrical outlets. The power supply is controlled from starters located in the relay room. The electrical connections will provide power to operate RRS_P-IA and IB. Two hoses, placed in the IIF, provide for transfer of sum water to the Reactor Vessel and are the interface with the RCS.

2.0 SYSTEM LIMITATIONS, SETPOINTS, AND PRECAUTIONS

- 2.1 To ensure proper cooling, the system pumps should not be operated at less then \$ gpm.
- 2.2 All hoses should be adequately supported/anchored to prevent whip when the pumps are sterted.
- 2.3 Bends in hoses should be minimized.
- 2.4 The system pumps should not be operated unless they are at least 2/3 submerged in weter.
- 2.5 The system pumps should be operated on a level surface in an upright position.
- 2.6 Prior to installing the RRS, personnel should be aware of the radiation levels in the wicinity of the 305' elevation hatch and the IIf.
- 2.7 Prior to pumping Meactor Building sump water into the Reactor Vessel, the following sequence of events should be performed:
 - add an appropriate quantity of boron, at determined by a mass balance, to the sump later to raise the sump boron concentration above 4350 pps.
 - p. mis the sump water by rectrculating a minimum of 3 sums volumes.
 - obtain and analyze sump samples to verify that the sump water borom concentration is greater than 4350 ppm.

3.0 OPERATIONS

3.1 Operation in the Turbine Building (Technical Specifications Surveillance)

This section provides instructions for periodic surveillance testing of the RPS and is intended only as a guide. If the DIA tank is unavailable for testing the RPS, another setup will be used.

3.1-1 Setup

RES.P-IA and RBS.P-IB, hose, and control menifold are removed from the staging area. All components are inspected for damage and replaced or repaired if required. A 100 foot section of the hose is connected to the discharge of each pump. Each pump is then rigged by its handle to the 1 ton gastry crane and lowered into the DIA tank until 12 rests on the bottom of the tank celevation 282'). The opposite end of the discharge hoses and pump electrical cords are retained on the turbine deck. The discharge hoses are connected to the inlets on the control manifold. A 5') foot section of hose is connected to each outlet on the manifold and the other ends are placed in the DIA. The electrical cords are connected to a emporary power-supply.

3.1.2 Normal Operation

Once the system is setup for testing, the breater is closed for the temporary power supply to energize RRS-P-1A and RRS-P-1B. Distance pressures are neasured at RRS-P-1A and RRS-P-1B and recorded at a flow rate of 200 gpm. The data is corrected for elevation and compared to the pump need curves to verify proper pump performance. Flow rate indication is provided by RRS-FI-IA and IB. During pump operation, hoise, fittings, and the control manifold are inspected for leakage. Repairs/Peplaceent of components is performed in the time frame specified in Reference 3.2.3.

The electrical outlels, located in the Reactor Sullding, are tested by energizing them in the relay room and measuring the voltage at the outlets.

3.1 3 Shutdown

When testing is completed, the pumps are stopped and removed from the DIA tank and the hoses are uncoupled and drained. All components are returned to the stading area.

3.2 Operation in the Reactor Building

This section provides guidance for setting up and operating the RPS during an unisolable Reactor Vesset leak.

3.2.1 Setup

If an unisolable Reactor Vessel leak occurs, RRS-P-1A, RRS-P-1B, the control manifold, and hose are removed from the staging area and transported into the Reactor Building to the hatch on the 305' elevation. A 50 foot section of distherge hote is connected to the mulck coupling on each own. Uting the holts provided for the robotics program, the pumps are lowered through the 305' elevation hatchway to the basement where they rest in a vertical, freestanding position. The other ends of the discharge hoses and the electrical cords remain on the 305' elevation. At this location, the distharge hoses are connected to the Inlets on the control manifold and the electrical cords are plugged into the previously installed dedicated electrical cords are plugged into the section of hose is connected to each manifold outlets. A 100 foot section of hose is connected to each manifold outlet and routed to the morthwest portion of the Reactor Guilding and placed in the session gas leading to the basement.

3.2.2 Normal Operation

1.2.2.1 Reactor Building Sump Recirculation

The starters, located in the relay room, are energized to start the pumps. The flow rate is adjusted to approximately 200 gap per pump at the control manifold. After three summ volumes have been rectrculated, summ samples are obtained and analyzed for boros, lenen the sump boron concentration exceeds 4350 ppm, the pumps are stopped.

3,2.2.2 Reactor Vessel/Sump Recirculation

Once the sump boron concentration is verified to be greater than 4350 ppm by a boron was balance calculation and a sample analysis, the two 100 foot hotes are removed from the seiseld qap, routed to the Reactor Vessel, and placed into the IEF. One or two pumps are started and throttled as required to match the Reactor Vessel leak. Periodic adjustments to this makeup rate are accomplished by starting and stopping the pumps from the relay room starters or by entering the Reactor Building and adjusting the throttle positions.

3.2.3 Shutdown

Makeup to the Reactor Vessel continues until the leak is stopped or until a permanent retirculation system is installed.

4.0 CASUALTY EVENTS AND RECOVERY PROCECURES

4.1 Casualty Events

the possible system casualty events during Reactor be sell sump recirculation include the following:

- a. loss of power to RRS-P-IA or RRS-P-IB
- b. fallure of RRS-P-IA or RRS-P-IB
- C. rusture of a hose
- d. transfer of out-of-specification water to the Reactor Yessel.

4.2 Design Features to Hitlgate Effects of Casualty Events

- 4.2.1 Power is supplied to the starters from a Class IE electrical system to meet the single failure criterion.
- 4.2.2 For leak rates of less than 200 gpm, only RRS-P-1A is required; RRS-P-1B provides the backup to met the single failure criterion. For leak rates exceeding 200 gpm, both pumps are required; the spare sump provides the backup to meet the single failure criterion.
- 4.2.3 Spare hose is available to replace a runtured or leaking hose.
- 4.2.4 Sampling capability exists in the system to prevent out-of-specification water from being discharged into the Reactor Vessel. In addition, the sump water will be mixed and borated as required prior to injection into the Reactor Vessel.

4.3 Recovery Procedures

- 4.3.1 Recovery from a loss of power to the pumps involves using the BMST for makeup until power is restored.
- 4.3.2 Recovery from a failed pump involves starting and throttling the remaining train and using the BMST for additional makeup as required until the failed pump is replaced.
- 4.3.3 Recovery from a rubtured hose involves starting and throttling the remaining train and using the BNST for additional makeup as required until the failed hose is replaced.
- 4.2.4 Recovery from a casualty event in which out-of-specification water is discharged into the Reactor vessel involves stooping the pumps, making up with the BMSI, and adding borom to the sump.

5.0 MAINTENANCE

5.1 Corrective Maintenance

- 5.1.1 Pump repairs shall be performed in accordance with Reference 1.2.4,
- 5.1.2 If repair welding is required to any pressure retaining component of the system, it shall be performed in accordance with the UNI used for initial construction. Upon condiction, the specific component shall be leak tested cer ANSI 831.1, 1983.

5.2 Preventive Haintenance

- 5.2.1 Preventive maintenance on the pumps is performed per the requirements of Reference 1.2.4.
- 5.2.2 Periodic calibration of the system flow and pressure indicators is performed in accordance with existing plant procedures.
- 5.2.3 All components are routinely inspected to spot potential problems.

5.3 Survetllance

Technical Specification Surveillance: are performed as described in Section 3.1 and in the time interval required by Reference 1.2.3.

5.4 In-Service Inspection

If the RRS is placed in operation per Section 3.2, all system components will be routinely imspected to spot potential problems.

6.0 TESTING

All system components, including the spare pump and hoses, are hydrostatically and functionally tested in accordance with AMSI 631.1, 1983 and plant procedures.

7.0 HUMAN FACTORS

- 7.1 All system components are labeled to ensure proper identification.
- 7.2 Dollys are used to transport heavy equipment.
- 7.3 All components are appropriately tagged to ensure they are not inadvertently removed from the staging area.

TABLE 1

REACTOR BUILDING SUMP RECIRCULATION PUMPS (RRS-P-1A, RRS-P-1B, SPARE)

Pump Details (see Figure 1 for Pump Performance Curve)

Identification MRS-P-1A, GRS-P-1B, SPARE

Hanufacturer Heda

Model No. L707G

Typo single stage vertical shaft centrifugal, submersible

Rated Speed, rom 3500

Rated capacity, gpm 265

Rated total dynamic head, feet 100 (at rated capacity)

Shutoff head, feet 260

Shaft Seal Ball bearing and double mechanical

seals

Lubricant Oil

Motor Details

Manufacturer Neda

Type Z-Pole, 3-Phase Induction 440V/20A

Enclosure Cast eluminum, AISI 17

мР 16,5

FIGURE 1

BEACTOR BUILDING SUMP RECERDILATION PUMPS (RRS-P-1A, RRS-P-1B, SPARE)

